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COMPLETE SPECIFICATION

Improvements in or relating to Fluid-Reaction Propelling Apparatus

I, Hans Endres, of 116 Kullerstrasse, Solingen, Germany, a German Citizen do hereby declare the nature of this invention and in what manner the same is to 5 be performed, to be particularly described and ascertained in and by the following statement:-

My invention relates to fluid-reaction

propelling apparatus.

It is an object of my invention to provide an apparatus of the kind described which may be used for vehicles on roads, for ships, or for power-generating plants of any kind, but is particularly useful in

15 the propulsion of aircraft.

The efficiency of the usual helical propellers for aircraft is very poor, and the speed they impart is comparatively low. Fluid-reaction propelling appara-20 tus as designed heretofore, i.e., with a single nozzle for ejecting a stream of compressed air, might be used for the propulsion of aircraft but their demand of compressed air is so high that the 25 power input is almost equal to that of a helical propeller. This is due to the fact that only about 5% of the kinetic energy in the stream of compressed air is utilized for propulsion, and about 95% is lost. 30 Apart from its low efficiency, the fluidreaction apparatus is preferable to the helical propeller on account of its simplicity. It does not require an elaborate power plant, with internal-35 combustion engines, reduction gears, etc., and does away with all the difficulties and risks of such a plant.

It is the principal object of my invention to so design a fluid-reaction pro-40 pelling apparatus that its efficiency is far superior to that of the single-nozzle apparatus referred to, as well as to the efficiency of the helical propeller while at the same time my novel apparatus is 45 almost as simple as the one with the

single nozzle.

To this end, I provide a jet, means for discharging a stream of fluid under pressure, normally compressed air, from the [Price 1/-]

jet, a nozzle surrounding the outlet open- 50 ing of the jet for conducting the stream into the open air, so that the stream produces a partial vacuum in the nozzle, and means controlled by the vacuum for producing the stream from the jet.

It is to be understood that in the following description the terms "front" and "rear," and corresponding expressions, relate to the direction in which the stream issues from the nozzle, i.e., this nozzle is at the rear end of the apparatus, and the jet from which the stream is primarily discharged, is in front of the nozzle.

Preferably, I provide a set of subsidiary nozzles between the nozzle at the rear end, or last nozzle, and the jet. The outlet pipes of the nozzles are arranged co-axially with respect to the jet, and to each other, and are so nested one within the other that the vacuum gradually increases and becomes a maximum in the first subsidiary nozzle. The areas of the annular clearances defined by the outlet pipe of the first subsidiary nozzle, and the outlet end of the jet, and by each pair of nested outlet pipes, increase progressively toward the rear of the apparatus, as required by the expansion of the streaming fluid.

In a preferred embodiment of my invention, I provide a compressor at or near the front end of the apparatus, and a piston which subdivides the compressor into a compression and a suction chamber. The jet is connected to the compression chamber, and the nozzle—or the first subsidiary nozzle, is connected to the suction chamber of the compressor. The piston is reciprocated by the difference of the pressures acting on opposite sides thereof, and controlled by means such as ports in its skirt, and corresponding ports in the wall of its cylinder.

My invention will be more fully understood from the following detailed description and the drawings in which three types of apparatus embodying my

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invention are illustrated by way of example.

In the accompanying drawings

Fig. 1 is an axial section, Fig. 2 is a rear-end elevation, Fig. 3 is a front-end elevation, and Fig. 4 is a section on the line IV-IV in Fig. 1; showing the first and simplest type in which a single compressor piston 10 is provided and a supply of compressed fluid, normally air, is controlled by the compressor piston, for starting,

Fig. 5 is an axial section, Fig. 6 is a rear-end elevation.

Fig. 7 is a section on the line VII—VII

in Fig. 1, and

Fig. 8 is a front-end elevation; showing the second type in which the compressor piston is subdivided into a principal 20 piston and a set of auxiliary pistons, all on a tubular piston rod, and the principal piston controls the supply of starting fluid,

Fig. 9 is an axial section, and

Fig. 10 is a rear-end elevation; showing the third type in which the compressor piston is subdivided, as in the second type, but the principal and auxiliary pistons are on a solid piston rod, and a 30 separate piston is placed on the rod for controlling the supply of starting fluid, Fig. 11 is an elevation of a ported

sleeve on the compressor cylinder,

Fig. 12 is an elevation of a ported 35 rotary valve for controlling the ports in the sleeve, and

Fig. 13 is an elevation of a cam for controlling the rotary valve, of the third

Referring now to the drawings, and first to Figs. 1 to 4, the parts of the apparatus are housed in a casing 1 whose rear end supports the last nozzle 2, with its outlet pipe 200. A compressor 45 cylinder 3 whose outside diameter is smaller than the inside diameter of casing 1, is screwed into the front end of the casing on whose edge it bears with a flange 4. 5 are bores in the wall of 50 cylinder 3 which, as shown in Fig. 4, are arranged on a circle about the axis of the cylinder, and are open to the atmosphere, or to the relative wind in the case of aircraft, at their outer ends while their 55 inner ends are connected to a row of ports 6 in the wall of cylinder 3. Another row of ports 7 arranged at the rear of ports 6, connects the interior of the compressor cylinder 3 to the annular space it 60 defines within the casing 1. Arranged still further to the rear is an annular groove 8 in the piston-swept inner surface

of the cylinder, and 9 and 10 are pipes

for supplying starting fluid, normally air

65 under pressure, to the groove 8 from a

suitable source, not shown. A plug 11 closes the compressor cylinder 3 at its front end, and a cover 12 is placed on its rear end. Inserted in this rear end is the base of a tapered jet 13, whose outlet end 130 extends to the rear. A casing 14 is also inserted in the cover 12 and supports a check valve 15 which opens into the cylinder 3, and spring 16 serves for seating the valve. A pipe 17 which extends through the wall of casing 1, is connected to the valve casing 14 at its inner end while its outer end opens into the atmosphere. The check valve 15 serves for admitting make-up air to the cylinder, as will be described.

Mounted to slide in the compressor cylinder 3 is a tubular piston 18 with a web 19 which subdivides the cylinder 3 into a compression chamber C at the rear, and into a suction chamber S at the front end of the cylinder. Rows of ports 66, 21 and 20 are formed in the skirt of the piston 18 for controlling, respectively, the rows of ports 6 and 7, and the groove It will appear that ports 66 and 21 are in the suction, and ports 20 are in the

compression chamber.

A spring 22 is placed in the suction chamber S within the tubular front portion of piston 18 upon whose web 19 its rear end bears. The front end of the spring is supported by a spring plate 23 at the inner end of a spindle 24 which is inserted in a female thread of plug 11 100 with its threaded portion, and equipped with a square portion 25 at its outer end for turning it and adjusting the tension of spring 22.

A set of subsidiary nozzles 26, with 105 outlet pipe 260; 27, with outlet pipe 270; 28, with outlet pipe 280; and 29, with outlet pipe 290; is inserted in the casing 1 between the jet 13 and the last nozzle The outlet pipes of the nozzles are 110 tapered and nested as shown, and their free sectional areas increase from the front toward the rear, the area of the outlet pipe 200 of the last nozzle 2 being largest. In the same proportion, the 115 annular spaces defined by two nested outlet pipes, increase toward the rear. The ratio at which the free sectional area of the nozzles increases, and the number of subsidiary nozzles provided, is 120 determined by the degree of expansion of the stream from jet 13. The bodies of the last nozzle 2 and of the subsidiary nozzles 26 to 29 are funnel shaped with curved walls, and their largest diameter 125 is equal to the inside diameter of casing 1. The volume of the compartments defined by two adjacent nozzles is a function of the ratio of the free sectional areas of their nested outlet pipes.

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It will appear that the outlet pipe 260 of the first subsidiary nozzle 26 surrounds the end 130 of the jet 13, the rear end 260 of the outlet pipe projecting beyond the 5 rear end 230 of the jet. The outlet pipe 270 of the second subsidiary nozzle 27 is in a similar position with respect to the outlet pipe 260 of the first one, and so on.

The compartments defined by the in-10 dividual nozzles are not connected to the atmosphere directly but only through the outlet pipe 200 of the last nozzle 2.

The operation of my apparatus is as

follows:

In the initial position of parts, as shown in Fig. 1, the spring 22 is fully expanded and the piston 18 is at the rear end of its stroke toward the compression chamber C. Its skirt lays open the ports 20 7 and the groove 8 but closes the ports 6. The check valve 15 in the rear cylinder

cover 12 is closed by its spring 16. For starting the apparatus, fluid under pressure, normally compressed air, is admitted to groove 8 through pipes 9 and 10. The air is admitted to the compression chamber C through the ports 20 in the skirt of the piston 18, produces a certain pressure in the chamber C and 30 flows out through jet 13, its pressure being transformed into velocity. The primary stream from jet 13 produces reaction and, through the nested outlet pipes 260, etc., accelerates the air in the compartments defined by the nozzles of the set, producing secondary flows. The partial vacuum produced by the primary stream from jet 13 is a maximum in the first nozzle 26. This vacuum which, due 40 to the cooperation of the several nozzles, may be lowered almost to an absolute vacuum, gets to the ports 7 in the cylinder 3, and, through ports 21 in the piston skirt, into the suction chamber S. The 45 reduction of pressure in suction chamber S, and the higher pressure in chamber C, cooperate to throw the piston 18 as far as the front end of its stroke, compressing

spring 22, closing ports 7 and groove 8, 50 and opening ports 6. Air, or relative wind, now enters the suction chamber S through bores 5, ports 6 and 66, and atmospheric pressure—or the pressure of the relative wind—is established in 55 suction chamber S. Spring 22 which had been compressed by the reduction of the pressure in suction chamber S, is now free to expand, and throws the piston 18 back to the rear end of its stroke, compressing

60 the air in compression chamber C and ejecting it through jet 13, until the piston 18 has returned into its initial position and the apparatus is ready for the next cycle. When the apparatus has been 65 started the supply of compressed air from

pipes 9 and 10 is throttled and reduced to the amount required for overcoming the frictional resistance of compressor piston 18, and for moving the piston into its final foremost position. Air for making up the volume required for producing the stream from jet 13 is drawn into the compression chamber C through check valve 15 when the piston moves in forward direction. The free sectional area of the check valve is overdimensioned to avoid return flow of air. The apparatus now keeps going until the supply of compressed air is cut off altogether. When this occurs the apparatus does not stop immediately but continues its operation for some time until the vacuum has become exhausted.

The theory of the apparatus will now be explained. When the starting air from pipes 9 and 10 has been throttled, as described, three flows of air are established in the apparatus as follows:

1. Drawing in make-up air through valve 15, this air which may be under the pressure of relative wind, is compressed in chamber C and discharged intermittently from jet 13 as the primary stream.

2. Access of the partial vacuum produced by the primary stream to suction chamber S and outflow of the air from such chamber.

3. Admission of relative wind to suction

chamber S through bores 5. The apparatus may be defined as a hollow member which is not accessible to atmospheric air directly. During the compression stroke of piston 18, air is expelled from the apparatus by the stream 105 from jet 13 issuing through the outlet pipe 200 of the last nozzle 2. During the make-up stroke of the piston, i.e., during its movement to the forward end of its stroke, the stream from pipe 200 is 110 interrupted and an indirect connection of the subsidiary nozzles to atmosphere is established but, due to the overdimensioning of check valve 15, there is no return flow of air through outlet pipe 200 and 115 the set of nozzles.

The kinetic energy of the stream from jet 13 is transformed into reduction of pressure in the nozzles. The partial vacuum thus produced is transferred to 120 suction chamber S, causing the pressure in compression chamber C to compress spring 22. When air, or relative wind, is admitted through bores 5, the spring 22 expands, throwing the piston 18 to the 125 rear and expelling the air from compression chamber C through jet 13.
When the piston moves in forward direction and compresses spring 22, makeup air is drawn into compression chamber 130

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C through check valve 15.

The principle of reaction propulsion on which my invention is based, is the production of pressure differences by gas 5 or air under pressure issuing from a nozzle, which differences become active as thrust forces. It is known from the theory of aviation that such differences of pressure acting on a surface, may be 10 very efficient. Thus, in a flying airplane, the pressure of the ambient air is reduced above, and increased below, the wings of the plane. The higher pressure acting on the wings in vertical direction 15 from below, produces the lift of the plane. By the reaction apparatus according to my invention, such pressure differences may be produced in horizontal direction, and high speeds attained, as 20 only the aerodynamic resistance has to be overcome. Reaction propulsion, as mentioned, is entirely practicable in air-craft, but has failed on account of its low efficiency.

I obtain high efficiency by utilizing the vacuum the stream from jet 13 produces, and, by providing a set of nozzles as described, the pressure in the individual compartments defined by the 30 nozzles is progressively reduced, the partial vacuum in each nozzle intensifying the partial vacuum in the other nozzle in whose outlet pipe the outlet pipe of the first-mentioned nozzle is nested, and the 35 partial vacuum produced may become almost equal to the absolute vacuum, as mentioned above.

This mode of operation is quite novel

and very efficient.

The only losses occurring in my apparatus are the friction losses in the jet, the nozzles and the compressor cylinder which may be estimated as 5%, and 95% of the available energy are utilized, as 45 against the helical propeller in which the major portion of the energy is wasted.

My invention revolutionizes the art of producing thrust for propulsion, and opens quite novel aspects in the develop-50 ment of airplanes. My novel apparatus is extremely simple as against the usual power plant of an airplane, is absolutely reliable and gives maximum efficiency, so that the highest speeds are attainable 55 therewith.

The paramount importance of my invention will be fully realized if it is considered that in my apparatus the relative wind is utilized very extensively for pro-60 ducing thrust force, which is impossible in a helical propeller as the circular area swept by its blades presents an extra resistance surface.

As the velocity increases, the relative 65 wind and the volume of air admitted to

the compression chamber C increase also, and it follows that the compression in the apparatus, and the thrust, increase with the velocity of the airplane or airship. Relative wind increases with the square of the velocity while reaction is directly proportional to velocity. There is a limit at which relative wind becomes equal to reaction, but this limit is a velocity much higher than the velocities attainable in propeller-driven aircraft.

Apparatus according to my invention are arranged at as many points of the aircraft, for instance, on the fuselage and the wings of an airplane, as may be required for eliminating one-sided stress on the parts, and for uniformly distributing the thrust forces. By regulating the individual apparatus, the production of reaction forces is adapted to existing fly-

ing conditions at any time.

In particular, my invention is very favorable for starting and landing, as, by turning the apparatus into vertical position, vertical forces are produced for lifting the airplane from the ground, and for decelerating its descent when landing. The lift is independent of the suction at the upper faces of the wings, and the necessity of providing long runs for starting and landing is eliminated.

My apparatus is first and foremost designed for the propulsion of aircraft but, as mentioned, it may also be used for propelling road vehicles and ships, and 100 for the operation of compressors and

similar machines.

Referring now to Figs. 5 to 8, the casing 1, with the rear nozzle 2, the subsidiary nozzles 26 to 29, to which a fifth 105 subsidiary nozzle 30, with outlet pipe 300, has been added, are arranged in the manner described with reference to Figs. 1 to 4, and the outlet pipes of the nozzles are nested, as also described. In this 110 type, however, the compressor cylinder is arranged in axial alignment to the casing 1 to whose front end it is secured by a flange 31, and the casing 1 and cylinder

3 are surrounded by a vacuum jacket 32. 115 The rear cover 12 is not placed on, but inserted in, the cylinder 3 ahead of flange 31, and cupped at its centre for the reception of jet 13. A piston valve 33 is mounted to slide with its boss on a 120 cylindrical portion of the jet 13, and provided with a row of ports 34. The piston valve 33 is forced against an inwardly projecting rim of flange 31 by a spring 36 and in this position of the piston 125 valve, its ports 34 register with ports 35 in the wall of the cylinder which connect the body of the first subsidiary nozzle 26 to the vacum jacket 32 through ports 34. The front end of spring 36 is supported 130

by the rear cover 12. Ports 37 connect the space between the piston valve 33 and the vacuum jacket 32.

The piston 18, with its web 19, but only 5 with the ports 20 and 66, is provided as described for controlling the groove 8 to which the starting-air supply pipes 9 and 10 are connected, and the ports 6 for admitting relative wind through bores 5.

In this type, however, the piston 18 is only the principal piston of a piston unit comprising, in addition to the principal piston 18, three auxiliary pistons 51, 52 and 53 which, together with piston 18, 15 are secured on a tubular piston rod 38. The front end of piston rod 38 which is larger than its rear end so that the rods

tapers like a nozzle, is equipped with a flange 39 bearing on the rear end of 20 spring 22 whose front end is supported by an annular flange 40 at the front end of cylinder 3. A tube 41 extends to the rear from flange 40 and an extension 42 of the piston rod 38 is fitted to slide in the

25 rear end of the tube.

In this type, make-up air is drawn in through the tubular piston rod 38. A cylinder 43 which is open at both ends, is inserted in the tube 41 and spaced 30 therefrom to form an annular air inlet passage 44. A transverse rib 45 closes the passage 44 at the rear and holds the cylinder in the tube. A piston 46 is mounted to slide in the cylinder 43, and 35 is forced against a check 48 at the rear end of the cylinder by a spring 47. In this position of the piston, ports 49 in the piston register with ports 50 in the cylinder 43 so that the air, or relative 40 wind, is admitted to the interior of piston rod 38 through passage 44, ports 49, 50 and the open rear end of the cylinder 43.

Three auxiliary pistons 51, 52, and 53 are secured on the hollow piston rod 38. 45 At the rear of every auxiliary piston, a partition 56, 56a and 56b, respectively, is arranged and secured in the cylinder 3 at its outer perimeter. The partitions are cupped toward their centres so as to 50 resemble nozzles, and their rear ends make a tight fit on cylindrical portions of the piston rod 38. Ports 57, 57a and 57b are formed in the piston rod 38 at the rear of each auxiliary piston. The front 55 end of the cylinder is closed by a partition or annular cover 58 which resembles the partitions 56 etc. The skirts of the auxiliary pistons have ports 54, 62 and 63, respectively, for cooperation with 60 ports 55, 59 and 60 which are connected to the bores 5.

The partition 58 and the first auxiliary piston 51 define together the first suction chamber Sa, and the piston 51 and the 65 partition 56 define together the first com-

pression chamber Ca. Similarly, piston 52 and partition 56 define the second suction chamber Sb, and piston 52 and partition 56a define the second compression chamber Cb. The third suction chamber Sc is defined by 56a and piston The third suction 70 53. The third compression chamber Cc is defined by piston 53 and partition 56b. The fourth suction chamber Sd is defined by partition 56b and principal piston 18, with its web 19, and the fourth com-pression chamber Cd is defined by the web 19 of piston 18 and by the rear cover 12 in which jet 13 is inserted.

Ports 7a connect the first suction chamber Sa to the vacuum jacket 32, and ports 7b, 7c and 7d similarly connect the

other suction chambers.

The operation of this apparatus is as follows:

In the initial position illustrated in Fig. 5, the piston valve 33, through ports 34 and 35, connects the body of the first subsidiary nozzle 26 to the vacuum jacket 32, ports 20 connect the groove 8 to the last compression chamber cd, and the ports 7a etc. are exposed by the skirts of the respective auxiliary pistons, and the skirt of principal piston 18, for connecting the suction chambers Sa etc. to the vacuum jacket 32. Piston 46 in cylinder 43 admits air to the interior of piston rod 38 which is connected to compression chambers Ca to Cc by the ports 57, 57a, etc. in the piston rod, and to compression 100 chamber Cd by the open rear end of piston rod 38. The ports 55 etc. for admitting air to the suction chambers, are closed by the skirts of the respective pistons.

The compressed air from pipes 9 and 10 105 starts the apparatus, as described with reference to Figs. 1 to 4. The stream issuing from jet 13 produces a partial vacuum which is transferred to the vacuum jacket 32 through ports 34, 35 in 110 piston valve 33. The jacket is connected to the space between piston valve 33 and cover 12 by ports 37, and to the individual suction chambers Sa etc. through ports 7a etc. The pressure in compression 115 chamber Cd which is partly transferred to the other compression chambers Ca to Cc through ports 57 etc., throws the pistons toward their foremost position, while spring 22 is compressed. The for- 120 ward or suction movement of the pistons closes groove 8 and interrupts the supply of compressed air to compression chamber Cd. The air under pressure flows out from the several compression chambers 125 through jet 13. When the stream from jet 13 ceases to flow, the piston valve 33 disconnects the ports 34 and 35. the pistons move in forward direction,

air or relative wind is admitted to the 130

individual compression chambers through passage 44 and the hollow piston rod 38. Ports 7a etc. are closed by the skirts of the respective pistons, and the partial vacuum still present in the suction chambers Sa etc. moves the pistons into their foremost position in which their skirts expose the ports 55 etc. so that air or relative wind from bores 5 is admitted 10 to the suction chambers and the partial vacuum therein is broken. Spring 22 is now free to expand and throws the pistons to the rear, compressing the air in the compression chambers. The compressed 15 air is ejected through jet 13 and, reacting on piston 46, causes it to close the airinlet ports 50. Finally, the parts return into their initial positions shown in Fig
5. and are ready for the next cycle.

By the combination of pistons and 20

nozzles in series, as described, the kinetic energy of the stream issuing from jet 13 is utilized for compressing the fluid in the apparatus and the loss of the system is When the 25 reduced to a minimum. apparatus has been started, the supply of compressed air through pipes 9 and 10 is throttled, as described, and the amount of air still required for keeping the 30 apparatus going, is quite small, as the energy of the stream is recovered with the exception of the friction loss.

Equalization of the vacuum in the nozzles with atmospheric pressure cannot 35 occur, as the individual impulses of the stream from jet 13 occur so rapidly that the action of the intermittent stream is practically equal to that of a continuous one, and return flow of air is prevented.

Referring now to Figs. 9 to 13, the casing 1 with its nozzles is designed exactly as described with reference to Figs. 5 to 8, apart from the fact that it has six subsidiary nozzles instead of five, 45 as in Figs. 5 to 8. Obviously, the number of the nozzles as well as that of the suction and compression chambers, may be varied as desired in any type of my apparatus.

The cylinder 3 is connected to the front end of casing 1 by flanges 31, and the cylinder and casing are surrounded by the vacuum jacket 32, as in the second type. The rear cover 12, the jet 13, and 55 the piston valve 33, are also designed as

in that type.

A tapered cowl 64 is placed on the cylinder 3 at the rear of ports 61 and a sleeve 80, with three rows of ports 81, 82, 60 and 83, is secured to the wider front end of cowl 64 at 77. The sleeve surrounds the front end of cylinder 3 in spaced relation and at its own front end supports a cover 79 by flanges 78. The piston 18 65 by which the starting air from pipes 9

and 10 is controlled, is mounted in an extra cylinder 64¹ on the cover 79. The rod of piston 18 is a solid member 65 and surrounded by spring 22 whose front end is inserted in a socket at the centre of cover 79 while its rear end bears against the first piston 67 of the set on rod 65. The set includes four pistons, 67, 68 69 and 70 which are not "auxiliary" pistons as they do not cooperate with a principal piston, the piston 18 being arranged at the opposite end of cylinder 3. pistons are annular members, each with a tubular boss 71, 72, 73, and 74, respectively which are spaced from the piston rod 65 and connected to it by spiders 75. The pistons, with partitions 76, 77 and 78 in the cylinder 3, define the suction chambers Sa to Sd, and the compression chambers Ca to Cd. The tubular bosses of the pistons make a sliding fit in the partitions. Ports 55, 59, 60 and 61 connect the interior of cylinder 3 to the interior of cowl 64.

A rotary valve 84, with three rows of ports 85, 86 and 87 in line with rows 81, 90 \$2 and \$3 of the sleeve 80, is inserted in the sleeve and, with its web 88, is mounted for rotation in antifriction bearings 92 and 93. The bearing 92 which is in front of the web 88, is supported by a spring 91 on the cover 79, and the rear bearing 93 is secured to a flange 90 at the front end of cylinder 3. A cam 94, with camming members 95 and 96 at opposite 100 ends, is placed on the tubular boss 71 of the first piston 67 so as to rotate thereon, and is equipped with a flange 97 for engaging the web 88 of rotary valve 84. A pin 98 is arranged at the rear, and a pin 105 99 is arranged in front, of the cam 94.

The cylinder 64 of the starting piston

18 has a row of ports 100 which open into a tube 102 surrounding the cylinder. This tube is connected to the chamber of 110 the rotary valve 84 by ports 103 in the

cover 79. In the initial position illustrated in Fig. 9, the ports 20 of piston 18 are in line with the groove 8, as described. 115 When starting air is admitted, the piston 18 moves in forward direction and pulls the set of pistons 67 etc. in the same direction. Spring 22 is compressed. The valve 84 is so positioned that its ports 120 85 register with the ports 81 of the sleeve 80, and its ports 87 with the ports 88 of the sleeve, while ports 86 and 82 are out of register. The forward movement of the set of pistons increases the volume of 125 compression chambers Ca to Cd, and air, or relative wind, is admitted to, and drawn into, the chambers through ports 81, 85 and the tubular bosses of the individual pistons. The suction chambers 130

Sa to Sd are connected to the vacuum jacket 32 through ports 55 etc., and ports 83, 87 of the sleeve and the rotary valve. The air from the suction chambers is evacuated through ports 55 etc. and into jacket 32, and the accelerating movement of piston 18 is assisted by such evacuation. the ports 34 of piston valve 33, and 35 of cylinder 3, are out of register so that 10 the vacuum in jacket 32 is not transferred

to the first subsidiary nozzle 26.

Shortly before the pistons arrive at the foremost end of their stroke, the rear edge of piston 18 exposes ports 100 so that the 15 air from cylinder 64 flows into the compression chambers through tube 102 and ports 103. At the same time, the pin 98 on boss 71 of piston 67 engages the camming member 95a and turns the 20 rotary valve 84 to close ports 81 and 83, and to open ports 82 of sleeve 80. Over-throwing of the valve 84 is prevented by the vertical edge 95b of the subsequent camming member 95. Air or relative 25 wind is now admitted to the suction chambers Sa etc. through ports 55 etc. and spring 22 now throws the pistons to the rear, compressing the air in the compression chambers Ca etc., and ejecting 30 it through jet 13 as described. Shortly before the pistons arrive at the rear end of their stroke, the rotary valve 84 is reversed by pin 99 engaging a camming face 96a on one of the camming members 35 96. The apparatus is now ready for the next cycle.

It will appear that the hollow bosses 71 etc. of the pistons 67 etc. make up a passage for the air admitted to the com-40 pression chambers Ca etc., which passage opens into the jet 13. Any suitable means may be provided for connecting the bosses to the piston rod, for instance, steel ribs, not shown. Obviously such 45 means must not interfere with the flow

of the air in the tubular bosses.

By the means described, the streams and forces established in the apparatus, i.e., the partial vacuum and the relative 50 wind produced by the stream from jet 13 and by the velocity of the aircraft, respectively, are controlled and utilized for producing thrust. The rotary valve 84 is rotated uniformly and its operation 55 is absolutely reliable, as the stress on the members of this simple valve gear is quite negligible as compared with the usual valve gears of internal combustion engines. A particular drawback of such 60 valve gears is that considerable masses must be speeded up during a very short period. This is why the usual valve gears are limited to speeds of the order of about 4000 revs. per min., much 65 higher speeds can be attained with the

rotary valve according to my invention. The velocity imparted to aircraft is limited only by the equalization of the reaction produced in my apparatus, and of relative wind, as explained above, and this limit is much higher than the normal speeds of airplanes and airships.

Having now particularly described and ascertained the nature of my said invention and in what manner the same is to be performed, I declare that what I claim

1. A fluid-reaction propelling apparatus, characterised in that a stream of fluid under pressure is discharged from a jet and into the open air through the outlet pipe of a nozzle arranged co-axially to the jet, so that a partial vacuum is produced in the nozzle, and this partial vacuum is utilised for producing the

stream from the jet.

2. An apparatus as under claim 1, characterized in that a set of subsidiary nozzles is arranged between the said principal nozzle which is at the rear end of the apparatus, and the said jet, and that the outlet pipes of the nozzles are arranged co-axially to the jet and to the outlet pipe of the principal nozzle, and so nested with respect to each other and to the jet, that the partial vacuum is gradually increased from the principal nozzle to the first subsidiary nozzle, and the highest vacuum in the first subsidiary nozzle is utilized for producing the 100 stream from the jet.

3. An apparatus as under Claim 1 or 2, characterized in that the diameter of the outlet pipe of the principal nozzle is the largest, and the diameter of the outlet 105 pipe of the first subsidiary nozzle is the smallest one, and that the diameters of the intermediate nozzles have inter-

mediate values.

4. An apparatus as under claim 3, 110 characterized in that the number of subsidiary nozzles, the ratio of the diameters of their outlet pipes, and the volumes of the compartments defined by the nozzles, are determined by the degree of expansion 115 of the stream, and by the ratio of the free sectional areas of the outlet pipes.

5. An apparatus as under claims 2, 3, or 4, characterised in that the outlet pipes of the nozzles are tapered, and their 120 bodies are curved and funnel-shaped.

6. An apparatus as under any one of the preceding claims characterised in that the jet is tapered and at its outlet end has the smallest diameter of the 125 system.

7. An apparatus as under any one of the preceding claims, characterised in that the parts of the apparatus are housed in a tubular casing and the nozzles are so 130

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arranged as to be closed against the access of atmospheric air by the issuing stream of fluid, and only the principal nozzle is open to the atmosphere through 5 its outlet pipe.

8. An apparatus as under any one of the preceding claims, characterised by means for preventing return flow of atmospheric air in the apparatus.

9. Apparatus as under any one of the preceding claims, characterised in that a compressor is provided for operating the

apparatus.

10. An apparatus as under claim 9, 15 characterised in that the compressor is equipped with a piston subdividing it into a compression and a suction chamber, the compression chamber being connected to the jet, and the suction chamber being,

20 under the control of the piston alternately connected to atmospheric air, or to relative wind, and to the partial vacuum, and that a spring is inserted in the suction chamber and compressed by the pressure

25 in the compression chamber, and expands to throw the piston toward the comchamber when the suction pression chamber is connected to atmosphere, or

relative wind.

11. An apparatus as under claim 10, characterised in that ports are provided in the cylinder and in the skirt of the piston by which the piston is automatically reversed from its foremost 35 position.

12. An apparatus as under claim 10, characterised in that ports are provided in the cylinder and in the skirt of the

piston for connecting the compression 40 chamber to a supply of compressed fluid in the foremost position of the piston, and for connecting the suction chamber to the partial vacuum in the rearmost position of the piston.

13. An apparatus as under claim 12, characterised in that the ports are so positioned with respect to each other that the supply of compressed fluid to the compression chamber is cut off, and 50 atmospheric air, or relative wind, is

admitted by another port into the suction chamber, in the rearmost position of the

piston.

14. An apparatus as under claim 12 or 55 13, characterised in that the passage for admitting the supply of compressed fluid to the compression chamber is partly constituted by a groove in the piston-swept inner surface of the cylinder.

15. An apparatus as under claim 10, or any one of claims 11 to 14, characterised by means for drawing make-up air into the compression chamber.

16. An apparatus as under claim 10, or any one of claims 11 to 15, characterised in that the compressor piston is subdivided into a set of individual pistons, and that each piston, with a partition in the cylinder, makes up a suction and a compression chamber in the

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cylinder.

17. An apparatus as under claim 16, characterised in that the individual pistons are secured on a hollow piston rod, and that the piston rod is provided with ports for admitting make-up air to the compression chambers, and with a valve controlled by the pressure variations in the piston rod and the compression chambers, for admitting the make-up air to the interior of the piston rod.

18. An apparatus as under claim 16, characterised in that make-up air is admitted to the compression chambers through tubular bosses on the pistons

surrounding a solid piston rod.

19. An apparatus as under claim 16, characterised in that a rotary valve for controlling the admission of make-up air to the compression chambers, and the connection of the suction chambers to atmosphere, or relative wind, and to the partial vacuum, is operatively connected to the pistons.

20. An apparatus as under claims 18 and 19, characterised in that a rotary camming member under the control of one of the tubular bosses is provided for operatively connecting the pistons to the

rotary valve.

21. A fluid-reaction propelling apparatus, substantially as shown in Figs. 1 to 4.

22. A fluid-reaction propelling apparatus, substantially as shown in Figs. 5 105 to 8.

23. A fluid-reaction propelling apparatus, substantially as shown in Figs. 9 to 13.

Dated this 15th day of August, 1934. HAROLD BARON 231, Strand, London, W.C.2. Chartered Patent Agent.

